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COMPUTATIONAL FLUID DYNAMICS

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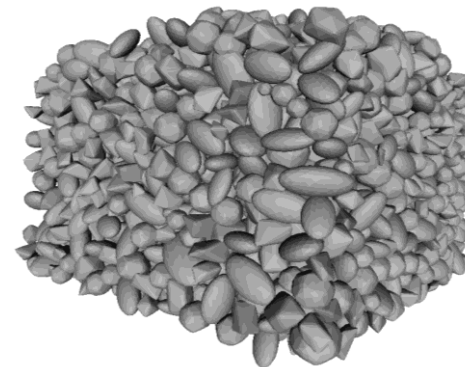
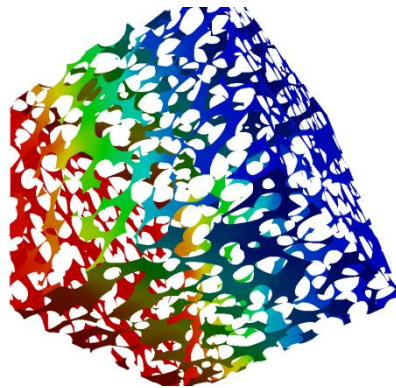
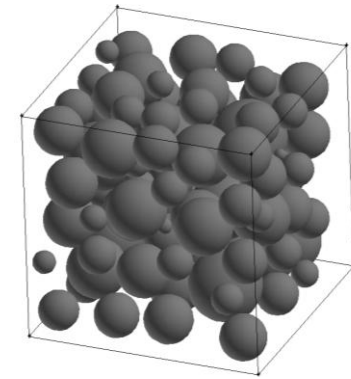
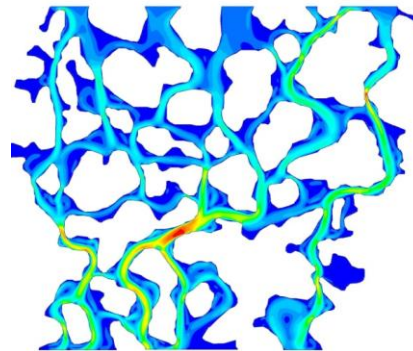
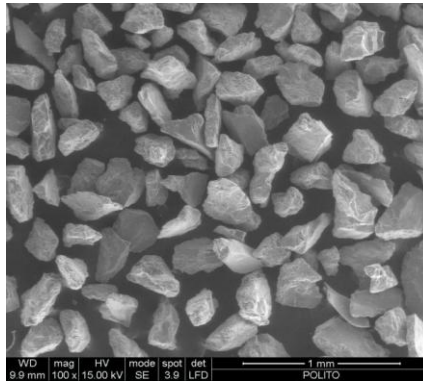
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SIMULATION OF FLOW AND PARTICLE TRANSPORT AND DEPOSITION IN POROUS MEDIA WITH COMPUTATIONAL FLUID DYNAMICS



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INTRODUCTION: MOTIVATION OF THE WORK

MANY FIELDS OF INTEREST:

- PROCESS ENGG.:
 - Packed bed reactors
 - Filtration
 - Chromatographic separation
- ENVIRONMENTAL ENGG.:
 - Aquifer remediation

PURPOSE

Results from
microscale simulations ...



... used to develop
macroscale models

“.. since, depending on the right scale of observation, everything is porous. “

THEORETICAL BACKGROUND: FLUID FLOW

MACROSCALE PSEUDO-CONTINUUM APPROACH

- Creeping flow ($Re < 1$): linear relationship

DARCY'S LAW
$$\frac{\Delta P}{L} = \frac{\mu}{k} q$$

- $Re > 1$: nonlinear relationship

FORCHHEIMER'S LAW
$$\frac{\Delta P}{L} = \frac{\mu}{k} q + \beta \rho q^2$$

- Packed beds filter law (wide range of Re)

ERGUN'S LAW
$$\Delta P^* = \frac{150}{Re^*} + 1.75$$

$$\Delta P^* = \frac{\Delta P \rho D_g \varepsilon^3}{L G_0^2 (1 - \varepsilon^3)}$$

$$Re^* = \frac{D_g G_0}{(1 - \varepsilon) \mu}$$

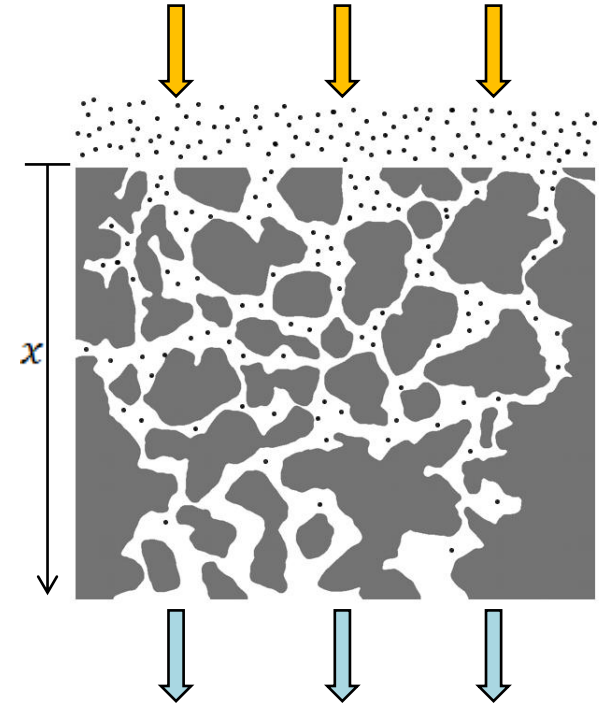
THEORETICAL BACKGROUND: PARTICLE DEPOSITION

MACROSCALE 1D ADVECTIVE-DIFFUSIVE EQUATION

$$\frac{\partial C}{\partial t} + q \frac{\partial C}{\partial x} - D \frac{\partial^2 C}{\partial x^2} = \textit{Source}$$

$$\textit{Source} = -K_d C$$

$$K_d = \frac{3}{2} \frac{1 - \varepsilon}{\varepsilon} \frac{q}{D_g} \alpha \eta$$



η : COLLECTOR DEPOSITION EFFICIENCY

THEORETICAL BACKGROUND: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY

- BROWNIAN DIFFUSION

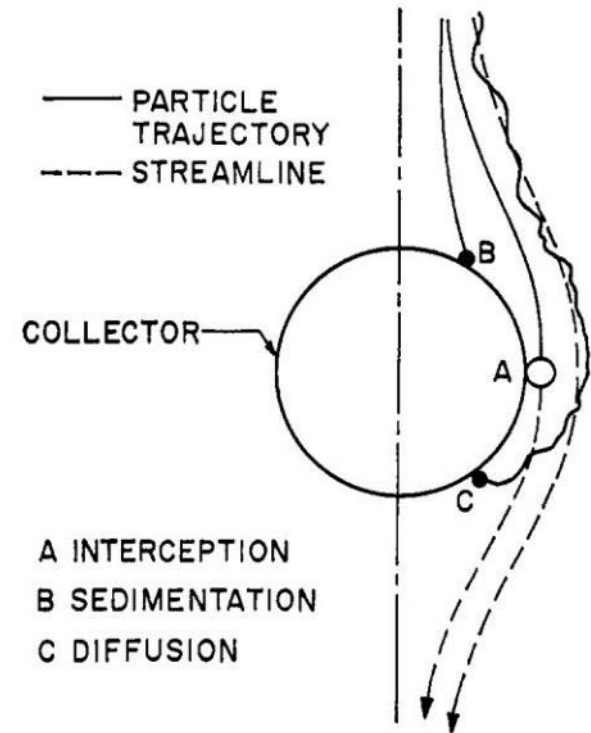
$$\eta_B = 4.04 Pe^{-\frac{2}{3}} \quad \text{LEVICH}$$

$$\eta_B = 4 As^{\frac{1}{3}} Pe^{-\frac{2}{3}} \quad \text{HAPPEL}$$

- INTERCEPTION

$$\eta_I = \frac{3}{2} \left(\frac{d_p}{D_g} \right)^2 = \frac{3}{2} N_R^2 \quad \text{YAO}$$

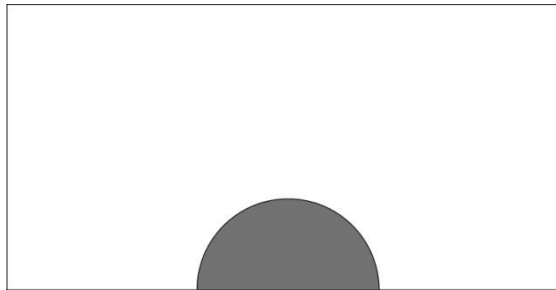
$$\eta_I = \frac{3}{2} As N_R^2 \quad \text{HAPPEL}$$



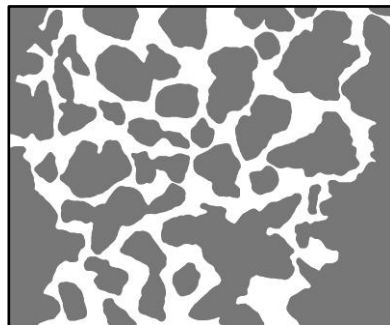
METHODOLOGY: MICROSCALE GEOMETRIC MODELS

INCREASING COMPLEXITY

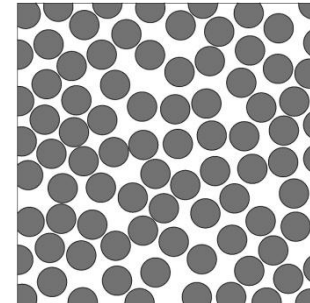
- SINGLE COLLECTOR
- CIRCULAR SHAPE
(under axial symmetry)



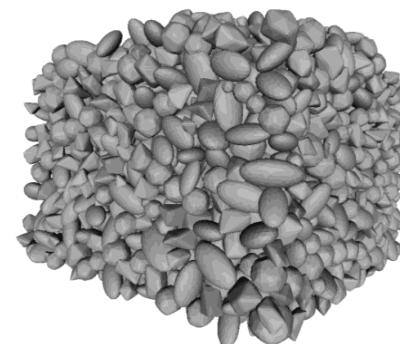
- IRREGULAR SHAPES
- REALISTIC μ -CT/SEM SCANS
(planar geometry)

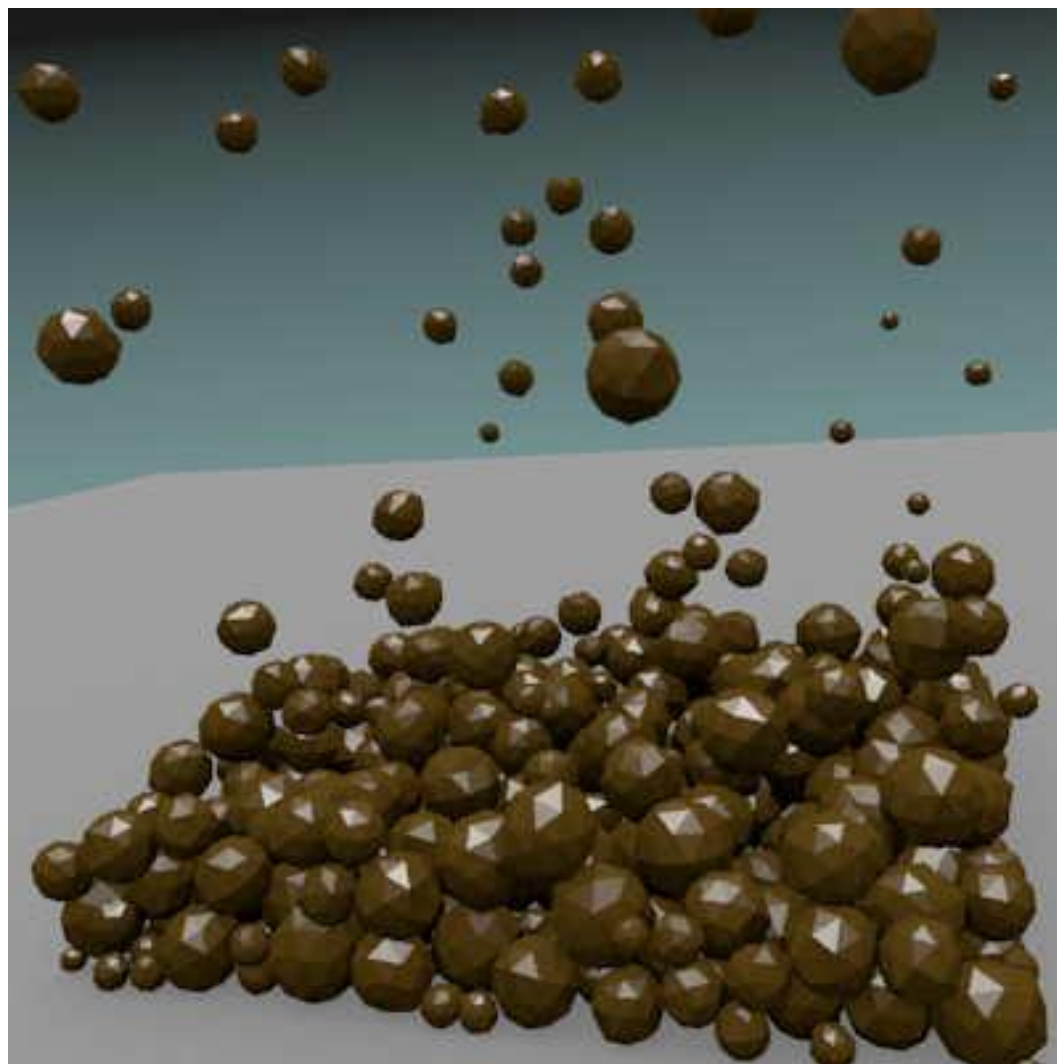


- CIRCULAR SHAPE
- ARTIFICIAL PACKING
(planar geometry)



- IRREGULAR SHAPES
- ARTIFICIAL PACKING





METHODOLOGY: OPERATING CONDITIONS

SOLVERS AND MESHING

- Finite volume CFD codes:

FLUENT, OPENFOAM

- Body-fitted meshers:

GAMBIT, SNAPPYHEXMESH

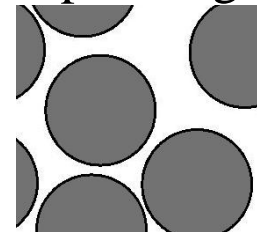
OPERATING CONDITIONS

- $D_g = 100 \text{ } \mu\text{m} \div 300 \text{ } \mu\text{m}$
- $\phi = 0,3 \div 0,5$
- $q = 10^{-6}, 10^{-5}, \dots, 10^{-1} \text{ m s}^{-1}$
- Laminar model
- $T = 293 \text{ K}$
- Viscosity $\eta = 0.00103 \text{ Kg m}^{-1}\text{s}^{-1}$

- 8 realistic geometries

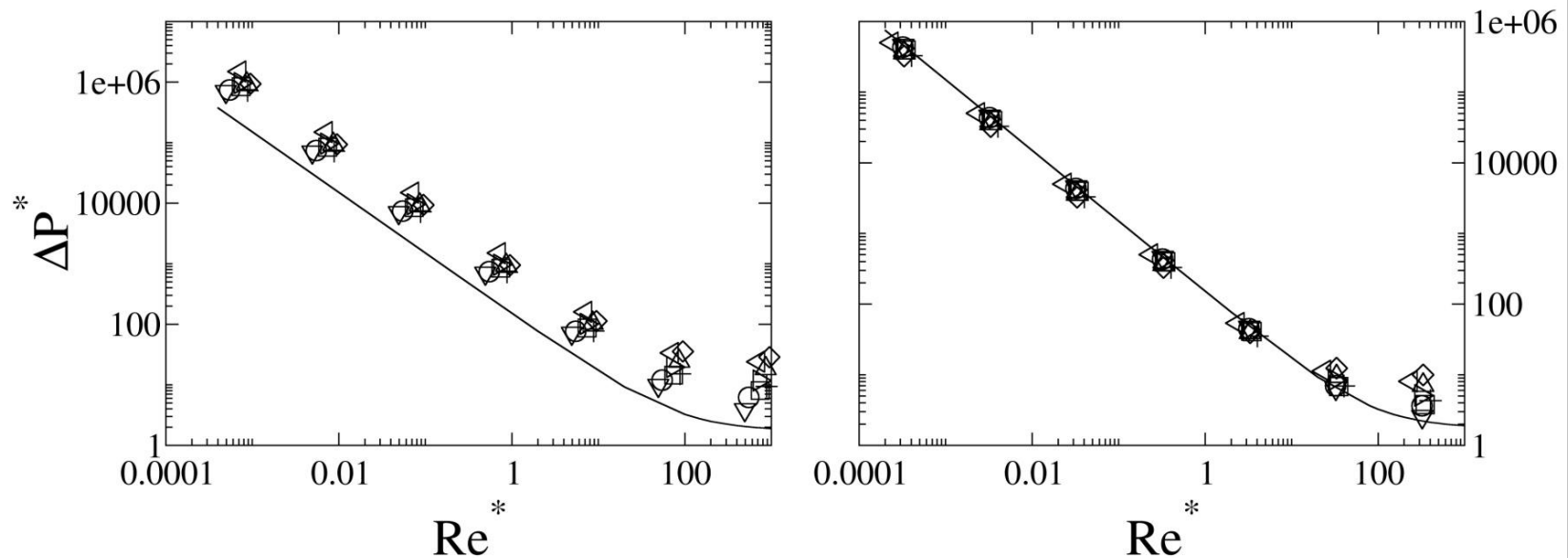


- 4 simplified geometries



RESULTS: FLUID FLOW

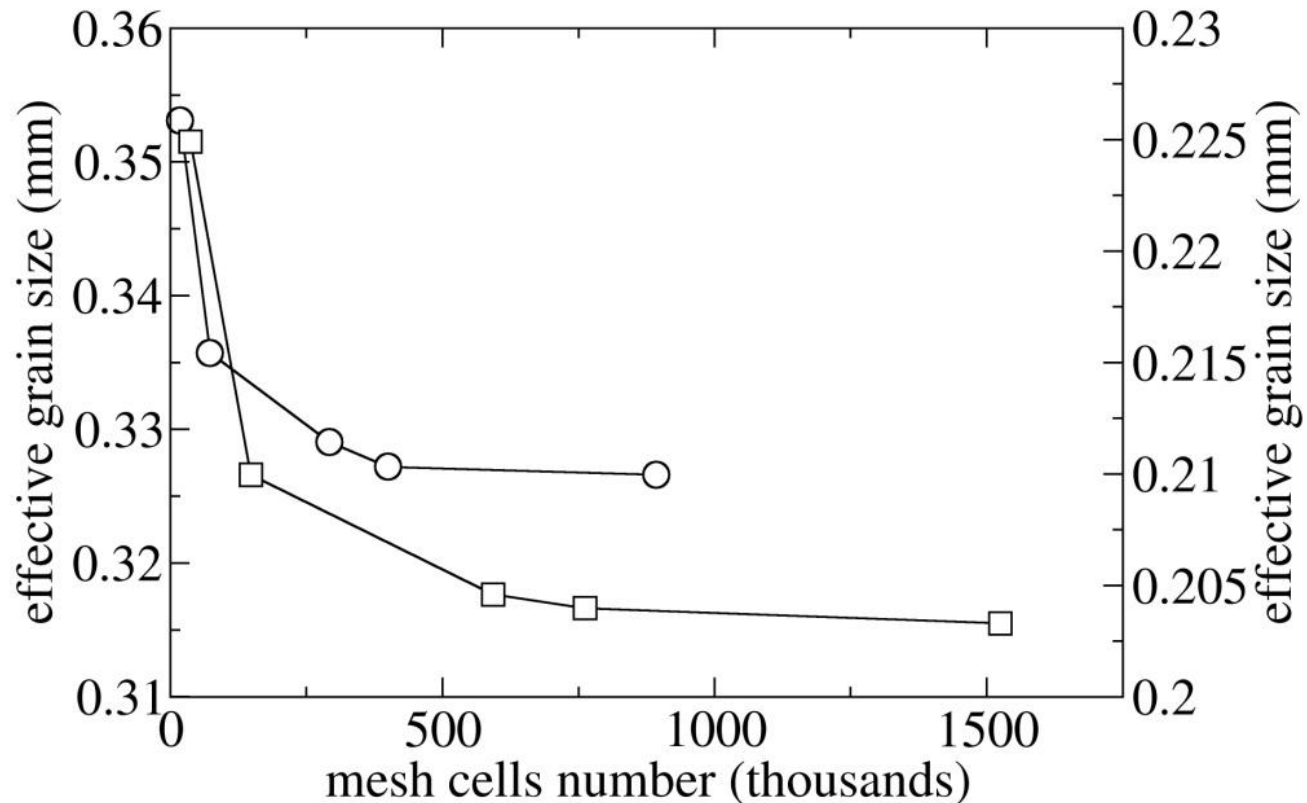
COMPARISON WITH ERGUN'S LAW



- Results show good agreement with Ergun's law
- Fitting on Ergun's law to obtain an effective grain diameter, D_g^*

RESULTS: FLUID FLOW

GRID INDEPENDENCE VERIFICATION

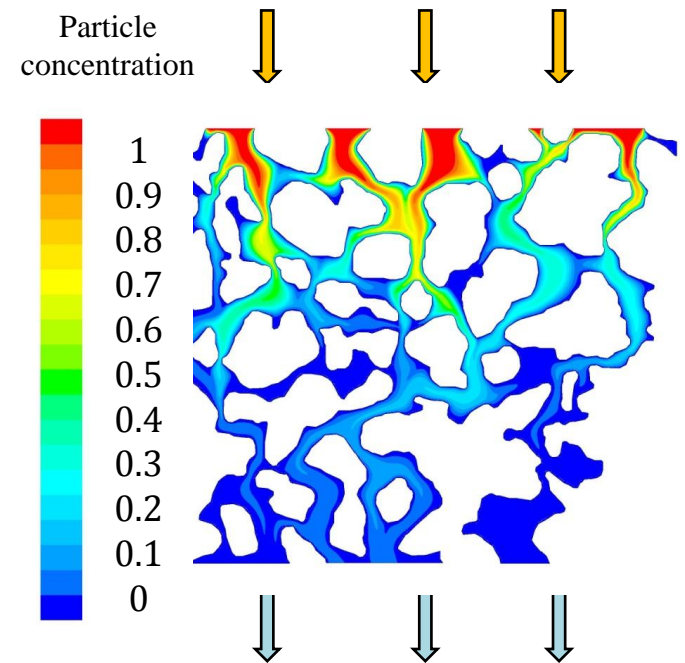


- Need for a single parameter summarizing fluid flow results
- Grid independence assessed with changes in D_g^*

METHODOLOGY: OPERATING CONDITIONS

PARTICLES MODELING

- Particles are transported by convective and diffusive phenomena
- $C = 1$ at inlet
- $C = 0$ on grain surface
 - Assumed “perfect sink” condition
- Particle diameter
 $d_p = 1, 10, 100, 200, 500, 625, 750, 875, 1000 \text{ nm}$

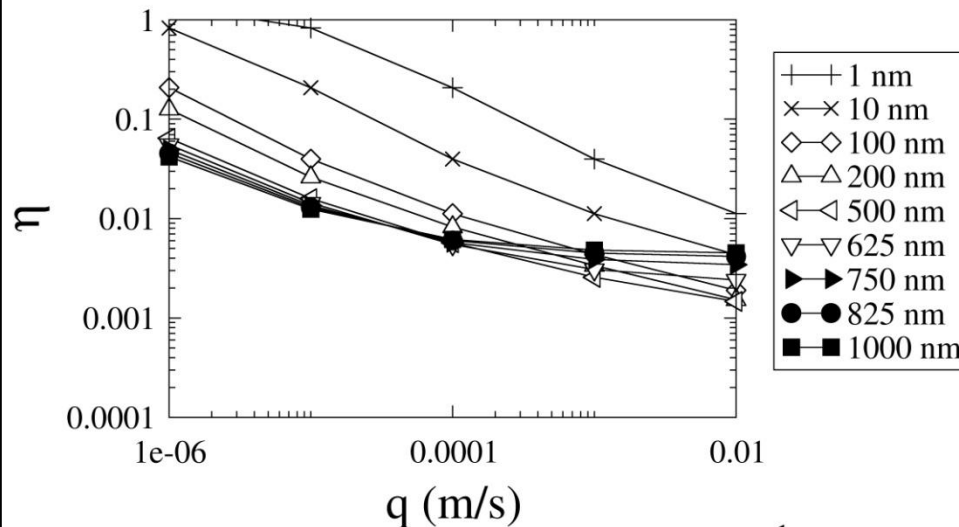


Collector deposition efficiency, η
calculated with packed bed performance equation

$$\frac{dC}{dx} = -\frac{3}{2} \frac{1 - \varepsilon}{\varepsilon D_g} \eta C$$

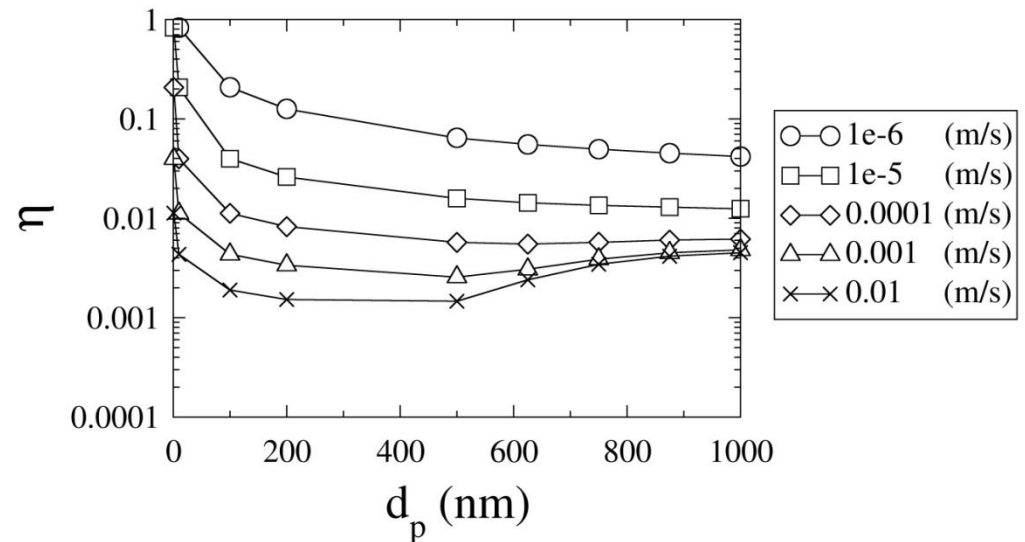
RESULTS: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY: OVERVIEW



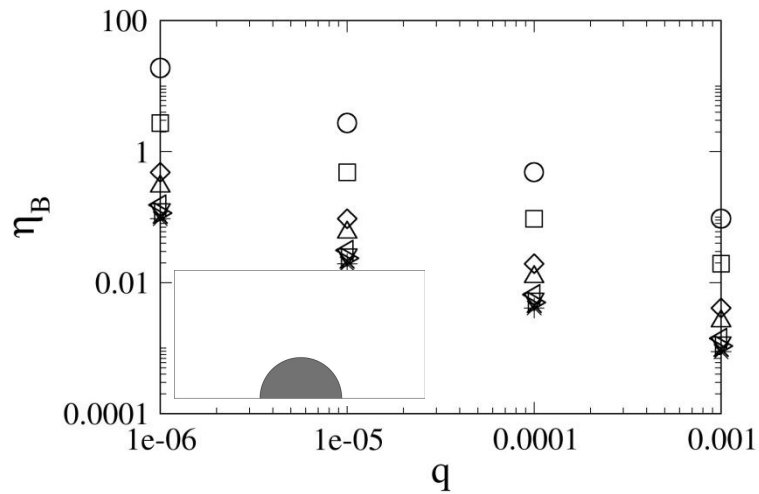
Efficiency η decreases for higher superficial velocities q (low residency times)

Efficiency η decreases for higher particle diameter (low diffusivity) until a certain d_p value, then increases for the steric interception effect.



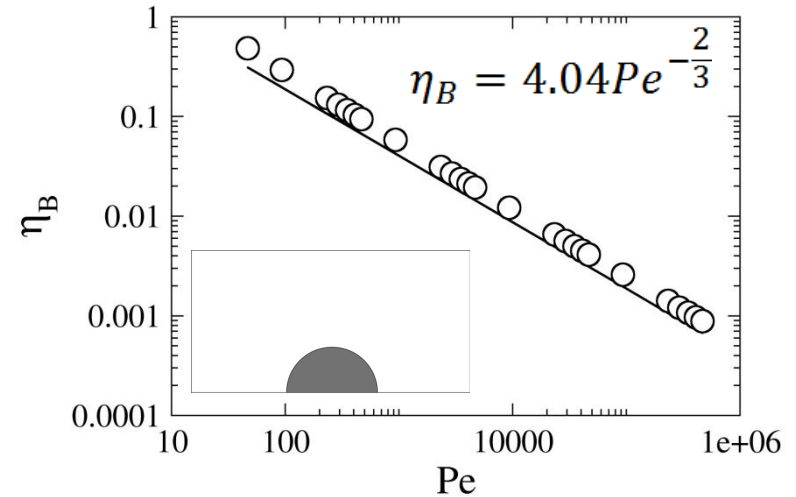
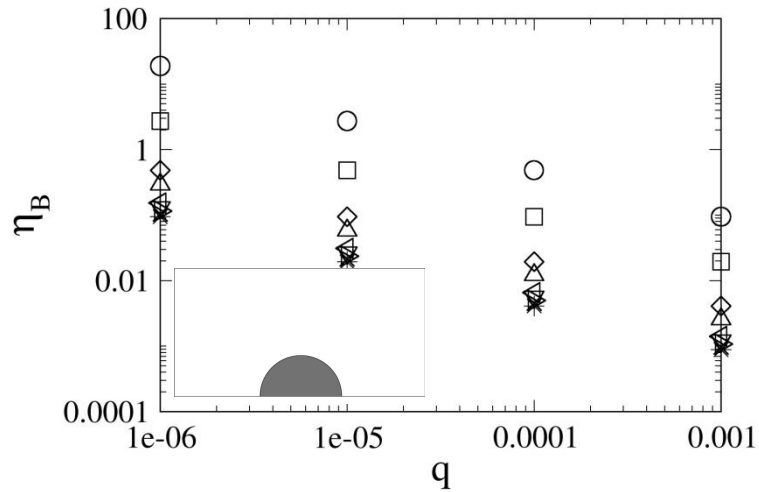
RESULTS: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION



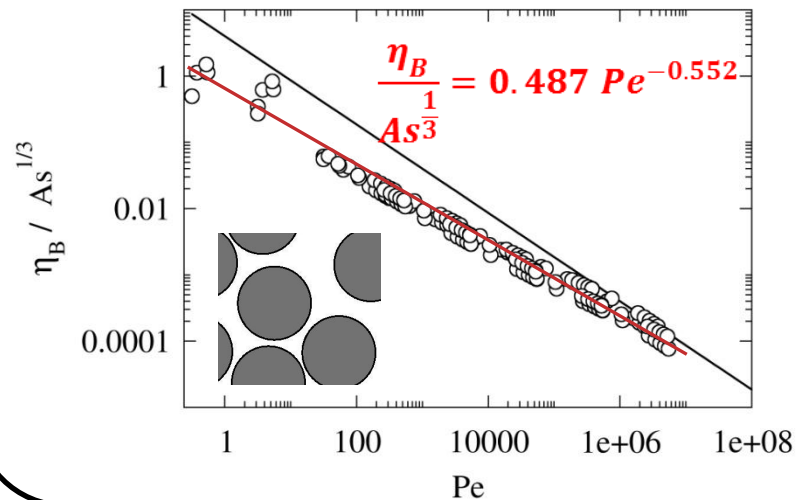
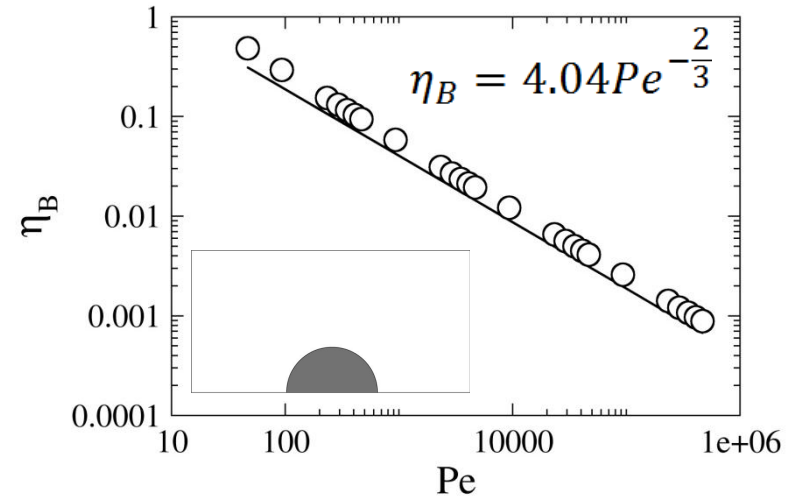
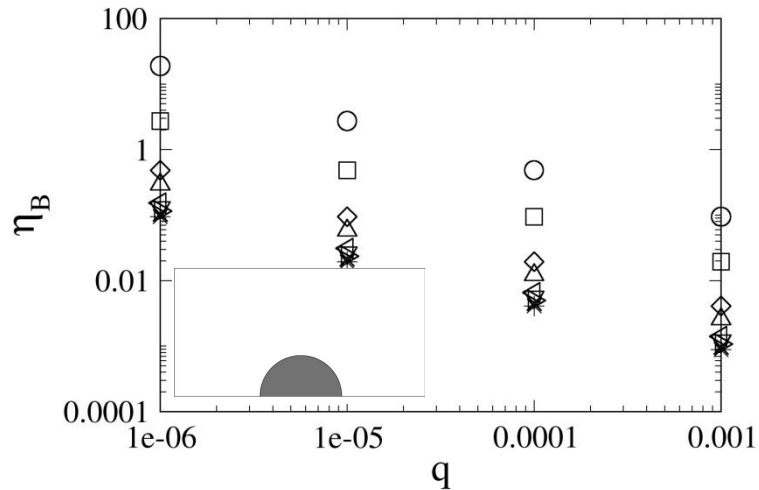
RESULTS: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION



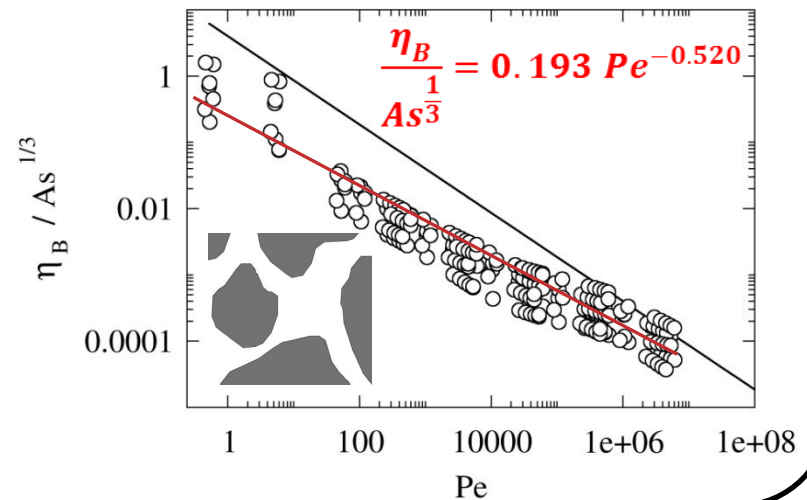
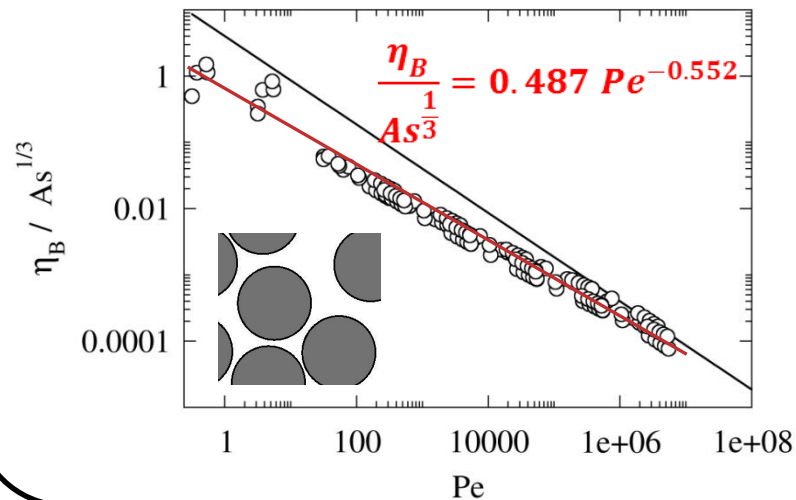
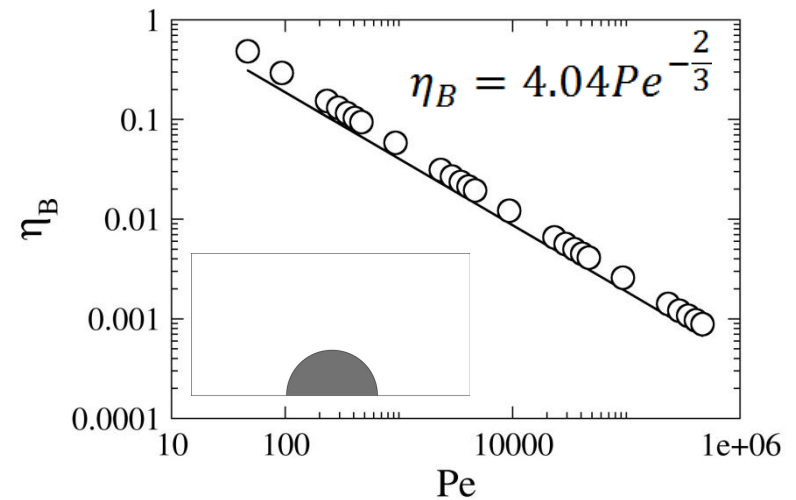
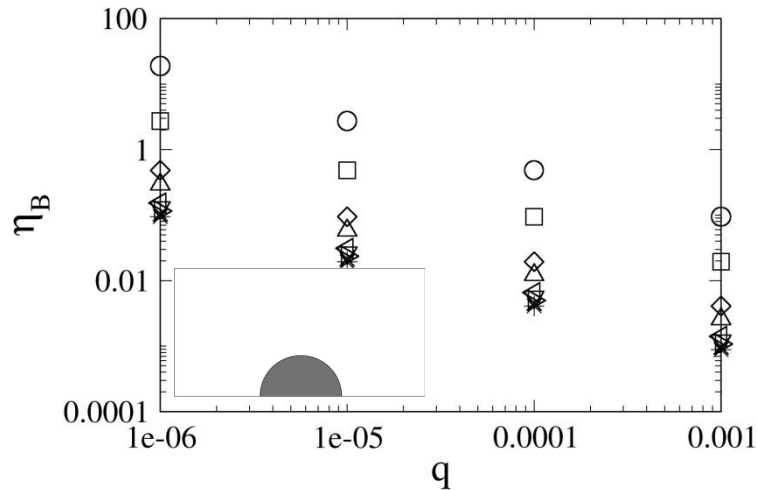
RESULTS: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION



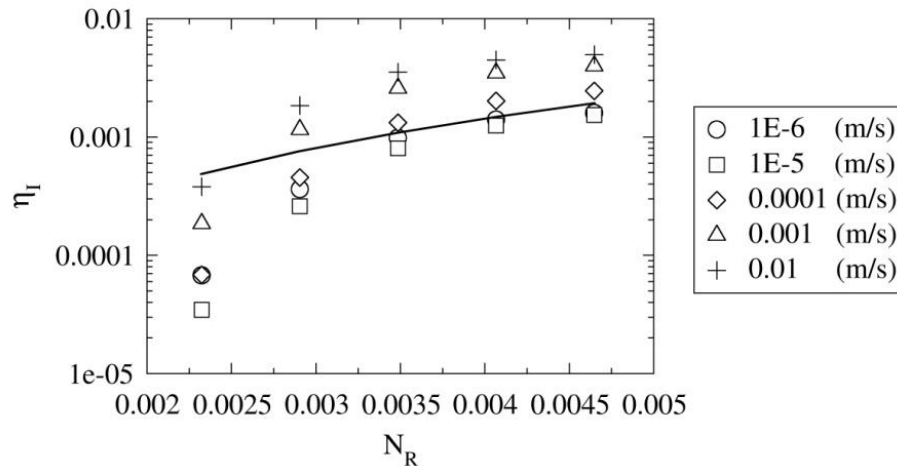
RESULTS: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION



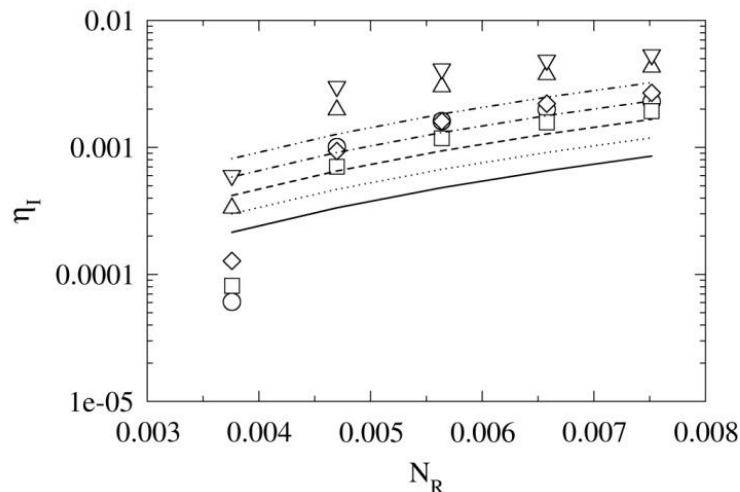
RESULTS: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY: INTERCEPTION



Theoretical law:

$$\eta_I = \frac{3}{2} As N_R^2$$



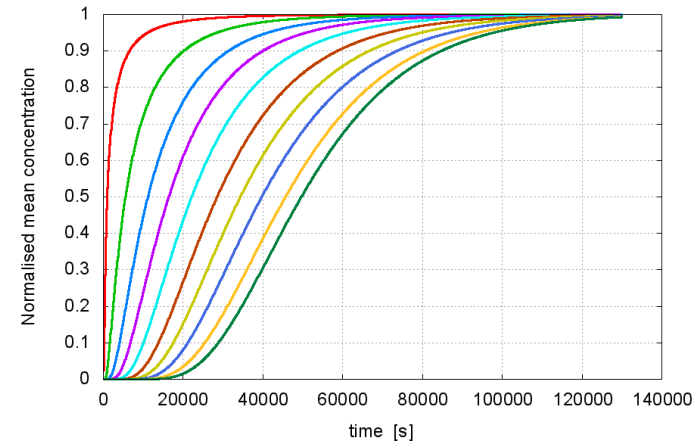
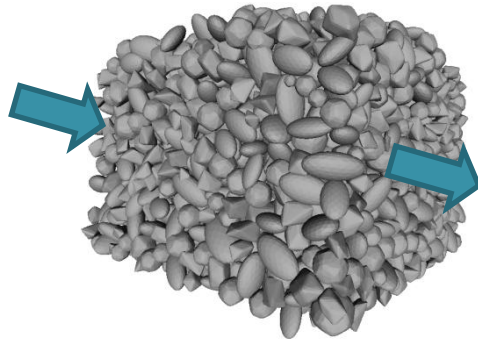
- Results appear in line with theoretical predictions but are strongly dispersed, with great variations at different q
- A dependency of η on q can be proposed



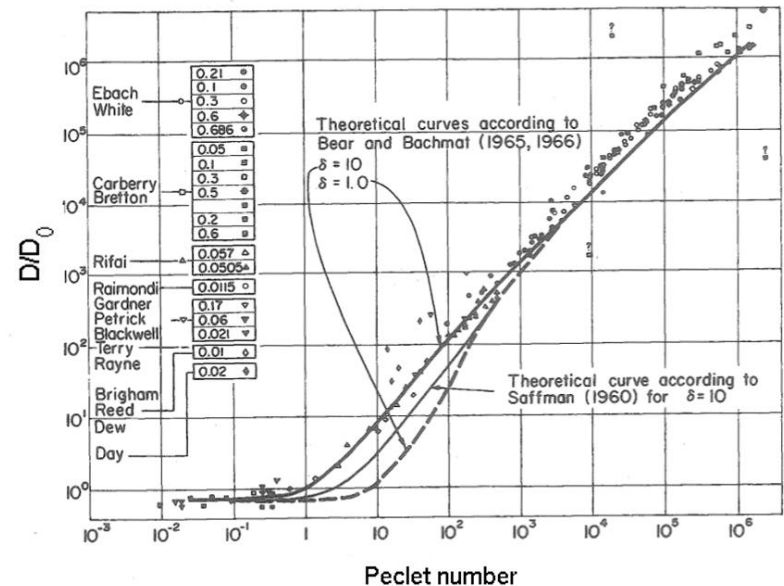
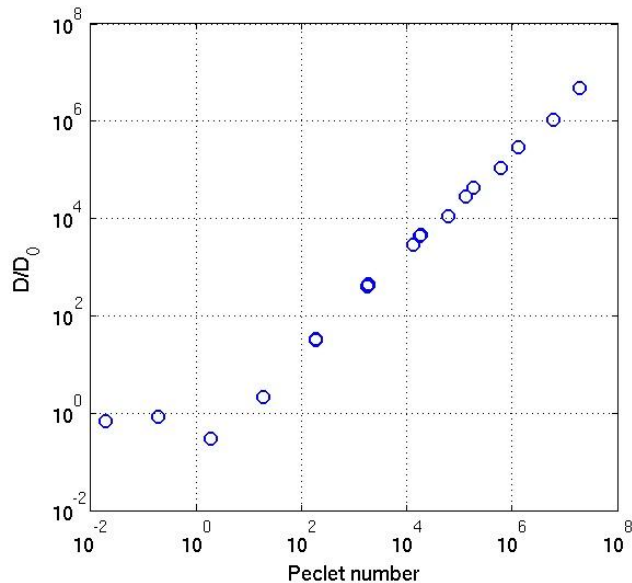
$$\eta_I = 3.377 As N_R^2 q^{0.145}$$

CONCLUSIONS AND FUTURE WORK

FULLY 3D PARTICLE TRANSPORT SIMULATIONS



Breakthrough curves fitting \longrightarrow Hydrodynamic dispersion $\mathcal{D}/\mathcal{D}_0$ results



CONCLUSIONS AND FUTURE WORK

ACKNOWLEDGEMENTS

- AQUAREHAB (FP7, Grant Agreement no. 226565)
- PRIN Project 2008:
“Disaggregazione, stabilizzazione e trasporto di ferro zerovalente nanoscopico”

Thanks for your attention!

Any questions?